

Method of numerical solution of nonhydrostatic equations of compressible atmosphere in the weather forecast problem

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Our purpose:

- New nonhydrostatic semi-lagrangian semi-implicit finite-difference dynamical core for the SLAV model.

SLAV:

- » is the global operational model in Russia (Tolstykh, 2010).
- » Based on the equations of hydrothermodynamics for the incompressible atmosphere in hydrostatic equilibrium.
- » Horizontal resolution for the Russian territory is assumed to grow by 2012 to 20km, whereas the number of vertical layers will be increased from 28 to 60.

Atmospherical equations

$$\frac{dU}{dt} + RT \nabla_{xy} \ln(p) + fk \times U = 0$$

$$\frac{dw}{dt} + g + RT \nabla_z \ln(p) = 0$$

$$\frac{dT}{dt} - T \frac{R \ln(p)}{c_p} = 0$$

$$\left(1 - \frac{R}{c_p}\right) \frac{\ln(p)}{dt} + D_3 = 0$$

$$p\alpha = RT$$

Hydrostatic approach:

$$\frac{dw}{dt} \ll g$$

ref. hydrostatic state: $\nabla_z \ln p_* = -\frac{g}{RT_*(z)}$

$$\begin{aligned}(\ln p)' &= \ln \frac{p}{p_*} & P &= RT_*(\ln p)' \\T' &= T - T_* & B &= g \frac{T}{T_*} - \frac{g}{c_p} T_* P\end{aligned}$$

(Thomas S. et al, 1998)

$$(\ln p)' = \ln \frac{p}{p_*} \quad P = RT_*(\ln p)'$$

$$T' = T - T_* \quad B = g \frac{T}{T_*} - \frac{g}{c_p} T_* P$$

$$\frac{dU}{dt} + RT \nabla_{xy} \ln(p) + fk \times U = 0$$

$$\frac{dw}{dt} + g + RT \nabla_z \ln(p) = 0$$

$$\frac{dT}{dt} - T \frac{R \ln p}{c_p} \frac{dt}{dt} = 0$$

$$\left(1 - \frac{R}{c_p}\right) \frac{\ln p}{dt} + D_3 = 0$$

$$\frac{dU}{dt} + \nabla_{xy} P = R_U$$

$$\frac{dw}{dt} + \left(\nabla_z - \frac{N_*^2}{g} \right) P - B = R_w$$

$$\frac{dB}{dt} + w N_*^2 = R_B$$

$$\frac{d}{dt} \left(\frac{P}{c_*^2} \right) + D_3 - \frac{g}{c_*^2} w = 0$$

- ♣ Left side contains material derivatives plus linear forcing terms associated with acoustic and gravity oscillations.

2-dim case (in vertical plane).

Terrain-following Z coordinate: $\nabla \rightarrow \delta$

$$\frac{du}{dt} + \nabla_x P = R_u$$

$$\frac{dw}{dt} + \left(\nabla_z - \frac{N_*^2}{g} \right) P - B = R_w \longrightarrow$$

$$\frac{dB}{dt} + w N_*^2 = R_B$$

$$\frac{d}{dt} \left(\frac{P}{c_*^2} \right) + D_3 - \frac{g}{c_*^2} w = 0$$

$$\frac{du}{dt} + \delta_x P = R_u$$

$$\frac{dw}{dt} + \left(\delta_z - \frac{N_*^2}{g} \right) P - B = R_w$$

$$\frac{dB}{dt} + w N_*^2 = R_B$$

$$\frac{d}{dt} \left(\frac{P}{c_*^2} \right) + (\delta_x u + \delta_z w) - \frac{g}{c_*^2} w = 0$$

Here are:

$$\delta_x = \frac{\partial}{\partial x_Z} - \frac{G_1}{G_0} \frac{\partial}{\partial Z}$$

$$\delta_z = \frac{1}{G_0} \frac{\partial}{\partial Z}$$

$$G_1 = \frac{\partial z}{\partial x_Z}$$

$$G_0 = \frac{\partial z}{\partial Z}$$

Semi-implicit scheme:

$$u^{n+1} = -\Delta t_+ \delta_x P^{n+1} + \hat{u}^n$$

$$w^{n+1} = -\Delta t_+ \left(\delta_z P^{n+1} - \frac{N_*^2}{g} P^{n+1} - B^{n+1} \right) + \hat{w}^n$$

$$B^{n+1} = -\Delta t_+ N_*^2 w^{n+1} + \hat{B}^n$$

$$\frac{P^{n+1}}{c_*^2} = -\Delta t_+ \left(\delta_x u^{n+1} + \delta_z w^{n+1} - \frac{g}{c_*^2} w^{n+1} \right) + \hat{P}^n$$

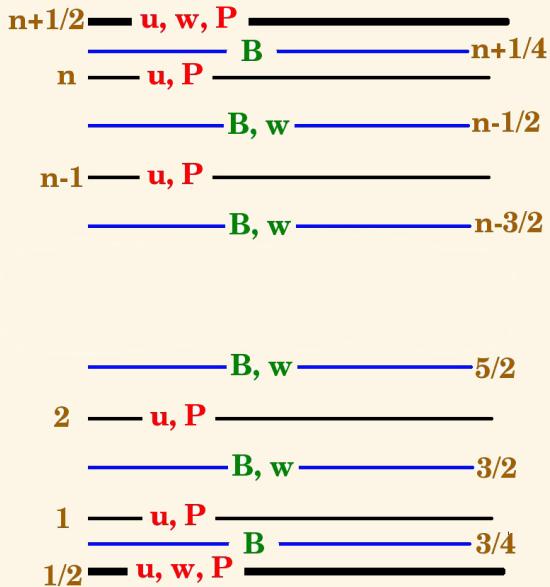
where $\hat{\cdot}$ values are known.

Main equation:

$$\begin{aligned} & \Delta t_+^2 (\delta_x^2 + e_0 \delta_z^2) P - \left(\frac{N_*^2}{g} + \frac{g}{c_*^2} \right) \delta_z P + \left(\frac{N_*^2}{c_*^2} - \frac{1}{c_*^2} \right) P \\ &= e_2 \left(\delta_z \hat{B} + \frac{1}{\Delta t_+} \delta_z \hat{w} - \frac{g}{c_*^2} \hat{B} - \frac{g}{c_*^2 \Delta t_+} \hat{w} \right) + \Delta t_+ \delta_x \hat{u} - \hat{P} \end{aligned}$$

$$\begin{aligned} e_2 &= \Delta t_{\pm} e_1 = \frac{(\Delta t_{\pm})^2}{1 + \Delta t_+^2 N_*^2} \\ \Delta t_{\pm} &= \Delta t \frac{1 \pm \epsilon}{2} \end{aligned}$$

Vertical structure of the model.



Boundary condition:

- $u_{1/2} = u_1$
- $w_{n+1/2} = 0$

$$\delta_x^2 = \delta_{2x}\delta_x$$

where

$$\delta_x = \tilde{\delta}_x - G^{13} \mu_x \tilde{\delta}_Z$$

$$\delta_{x2} = \tilde{\delta}_x + \frac{\bar{g}^{13}}{H} \mu_x - \frac{1}{G^0} \tilde{\delta}_Z G^1 \mu_x$$

so:

$$\delta_x^2 = \delta_{x2}\delta_x =$$

$$\begin{aligned} & \tilde{\delta}_x^2 - \tilde{\delta}_x G^{13} \mu_x \tilde{\delta}_Z + \frac{\bar{g}^{13}}{H} \mu_x \tilde{\delta}_x - \frac{\bar{g}^{13}}{H} \mu_x G^{13} \mu_x \tilde{\delta}_Z \\ & - \frac{1}{G^0} \tilde{\delta}_Z G^1 \mu_x \tilde{\delta}_x + \frac{1}{G^0} \tilde{\delta}_Z G^1 \mu_x G^{13} \mu_x \tilde{\delta}_Z \end{aligned}$$

Equation on the surface.

Vertical velocity:

$$\text{in } \mathbf{Z}: W_{i,1/2} = 0$$

$$\text{in } z: w_{i,1/2} = G_{1,i,1/2} u_{i,1/2} = G_{1,i,1/2} u_{i,1}$$

On the intermediate $k = 3/4$ level:

$$w_{i,3/4} = -e_1(\delta_z P - N_*^2/gP)_{i,3/4} + e_1 \hat{B}_{i,3/4} + e_0 \hat{w}_{i,3/4}$$

at the same time

$$w_{i,3/2} = -e_1(\delta_z P - N_*^2/gP)_{i,3/2} + e_1 \hat{B}_{i,3/2} + e_0 \hat{w}_{i,3/2}$$

$$w_{i,1/2} = G_{1,i,1/2} u_{i,1} = G_{1,i,1/2}(-\Delta t_+(\delta_x P)_{i,1} + \hat{u}_{i,1})$$

linear interpolation scheme:

$$w_{i,3/4} = aw_{i,3/2} + bw_{i,1/2}$$

\Rightarrow independent equation for $P_{i,1/2}$ based on the nonhydrostatic equation and surface boundary condition.

Equation near the top.

Top boundary condition:

$$w_{i,n+1/2} = W_{i,n+1/2} = 0$$

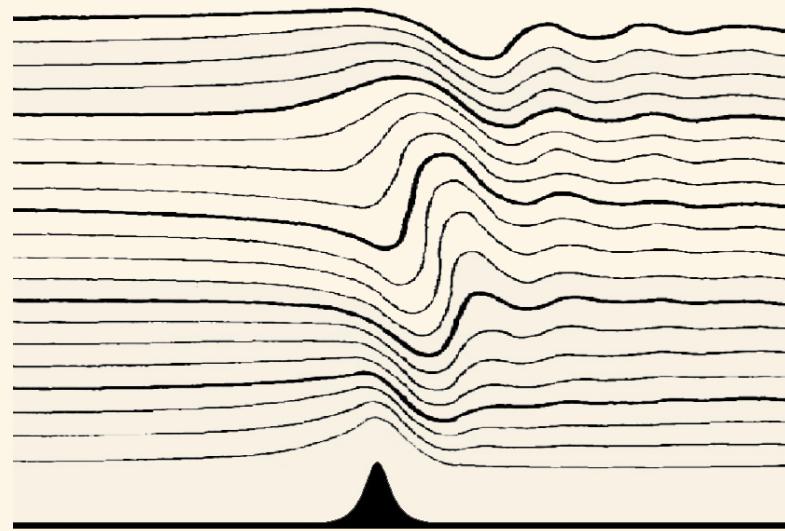
Hydrostatic approach on the $n + 1/4$ level:

$$(\delta_z \ln p)_{i,n+1/4} = -\frac{g}{RT_{i,n+1/4}}$$

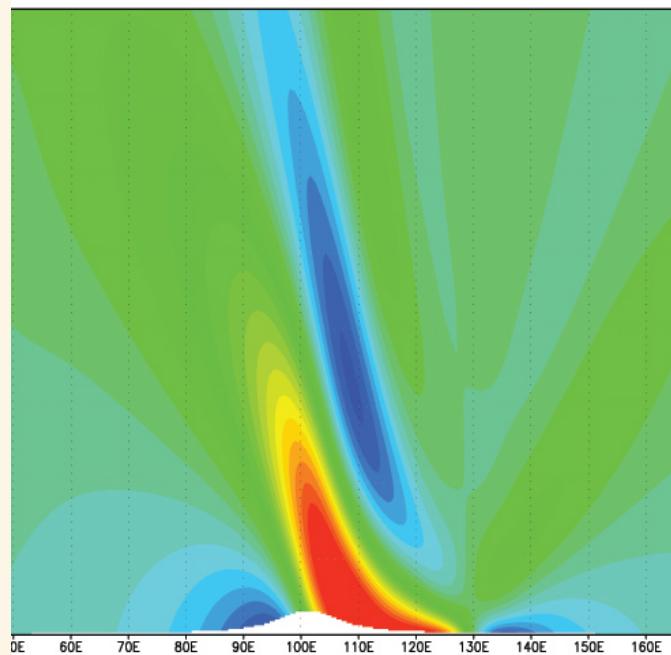
Equation for the $P_{i,n+1/4}$:

$$(\delta_z P)_{i,n+1/4} = g \frac{T_{i,n+1/4} - T_*}{T_{i,n+1/4}} = \frac{b_{i,n+1/4}}{1 + b_{i,n+1/4}/g}$$

Experiment: orographic waves.



velocity deviation (u).



- $dx=550m$, $dz=150m$
- $u=10 \text{ m/s}$
- $h=300m$

Conclusion:

- We developed the numerical method of the solution of nonhydrostatic equations.
- Further we plan to construct 3-dim nonhydrostatic dynamical core for the SLAV model.

Thank you for attention!